Simulation of Couplers

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Agenda

- Introduction to Couplers
- Traditional Simulation using LPM
- FEM/BEM Simulation
- Comparison of Results
- Conclusion



Introduction to Couplers

Critical properties of Acoustic Couplers

- Must allow for REPEATABLE measurements
- Must be possible to CALIBRATE
- Must be ACCURATE and STABLE
- Should be STANDARDIZED



- Design to improve voice quality & intelligibility
- Design to meet telecom & audio standards
- Comparison of transducers, headsets, handsets, earphones etc.



Acoustic Couplers overview

- IEC 318 (ITU-T P.57 Type 1) Ear Simulator
- IEC 711 (ITU-T P.57 Type 2) Ear Simulator
- ITU-T P.57 Type 3.1 Concha bottom Simulator
- ITU-T P.57 Type 3.2 Simplified Pinna Simulator
- ITU-T P.57 Type 3.3 Pinna Simulator

Increasing realism & complexity



Ear Anatomy and Definitions



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ITU-T Type 2 - IEC 711 occluded ear simulator

- Standardized accepted as a reference worldwide
- Bruel & Kjær Type 4157 (and used in 4158/59/95)
- Intented for calibration of insert earphones, sealed and unsealed (hearing aids) in the frequency range from 100-7.000Hz
- Simulates the ear canal from app. 10mm behind EEP and in







- IEC 711 coupler:
- Requirements in according to standard:
- Acoustical transfer impedance specified
- Equivalent volume at 500Hz equal to 1.26cm3
- With of principal volume 7.5mm
- Length of principal volume must produce ½-wavelength resonance at 14kHz, i.e. ~12.4mm









IEC-711 coupler typical measured data with tolerance curves from IEC60711









Ear drum impedance:

Two slits terminated by volumes, i.e. RLC-helmholtz resonators tuned to match drum-impedance







Ra7

Ma7

983.8

Ca7

2.1e-12

31.1e6









IEC	7.11.coupler			
Ma4. 82.9	· · · · · · · ·	Ma6. 130.3 .	· · · · · · · · · ·	Ma8, 133,4
		50,6e6		<pre>></pre>
$1S \xrightarrow{I} X \xrightarrow{I}$	0.943e-12	Ma5 = = 9.4e3	Ca6 1 1	Ma7 983.8
. <td></td> <td>Ca5 1.9e-12</td> <td></td> <td>Ca7</td>		Ca5 1.9e-12		Ca7
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Transfer impedance simulation (LPM)

IEC-711 coupler: Measured data and simulated data using LPM





Standard FEM Simulation

- Numerical model solving the Helmholtz equation inside the coupler
- Models the air inside without visco-thermal effects (loss-free)
- Allows for computation of acoustic modes (frequency and mode shape)





Transfer impedance simulation (FEM)





Visco-Thermal fluid

- Thermal conductivity and viscosity play a role near the boundaries
- The thermal & viscous mode only exist within a small boundary layer
- In large spaces, the acoustic mode dominates





Visco-Thermal FEM

- Finite Element model based on the narrow gap equation
 - const. pressure/zero particle velocity in thickness direction
 - small gap width compared with acoustic wavelength
- No need to mesh in the thickness direction
- Includes visco-thermal effects





Visco-Thermal FEM – Test Case





2D FE model of Slit





Simulation on Slit

• Acoustic input impedance – FE simulations vs. lumped-parameter model





Coupler Model

• Mixed FEM/BEM model (4818 elements & 2337 nodes)





Model Setup



Response point (for transfer impedance simulation)



Coupler Response @ 1000 Hz

Sound pressure map





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Frequency Response





- A complete BEM/FEM model of the IEC 711 coupler (B&K Type 4157) taking visco-thermal effects into account was presented.
- Comparison between a measurement and simulation of the transfer impedance show excellent agreement.
- A more correct and detailed 3D simulation of the coupler can be done using BEM/FEM compared to traditional LPM.
- The performance of virtual couplers can be evaluated at the very early design stage using the proposed BEM/FEM technique.



Any Questions ?



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